





East Sussex County Council Transport and Environment

Bexhill to Hastings Link Road S07 Combe Haven Underbridge Approval in Principle

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1. HIGHWAY DETAILS

1.1 Type of highway

Over: Bexhill to Hastings Link Road (BHLR) which is a single carriageway 2-lane rural all

purpose road. 12.0m carriageway with 2.5m verge on the east side and 2.5m verge

on west side.

Under: N/A

1.2 Permitted traffic speed

Over: 60 mph (96 kph)

Under: N/A

1.3 Existing restrictions

None

2. SITE DETAILS

2.1 Obstacles crossed

The bridge crosses Combe Haven Stream which flows from west to east. The channel width, measured between the tops of opposing banks is approximately 7.40m at its widest point below the footprint of the structure.

3. PROPOSED STRUCTURE

3.1 Description of structure

The structure is a single span underbridge carrying BHLR over Combe Haven Stream. The deck consists of inverted prestressed concrete T-beams with concrete infill. The deck is integral with reinforced concrete abutment walls supported on a piled foundation. The reinforced concrete wingwalls are set perpendicular to the abutment walls.

The parapet stringcourse will be cast in situ reinforced concrete.

The OS grid reference for the structure is 574843.8E, 110012.5N.

3.2 Structural type

The structure is a single span integral bridge designed as a frame-type integral bridge in accordance with BA 42/96.

Wingwalls cantilever from the rear of the abutment.

3.3 Foundation type

Reinforced CFA concrete piled foundation.

3.4 Span arrangements

Single clear span of 11.4m with zero skew

3.5 Articulation arrangements

The structure is an integral bridge which does not require deck articulation or movement joints. BD33/94 Type 2 (Asphaltic plug) joints are proposed at the approach

embankment/deck interfaces.

Thermal movement of the bridge deck is resisted by passive earth pressure behind the abutment wall and rotational stiffness of the end supports.

3.6 Types of road restraint systems

The proposed road restraint system requirement has been confirmed by a RRRAP assessment. A metal N2/W4 vehicle parapet 1000mm high with mesh infill will be provided to comply with the requirements of TD19/06.

3.7 Proposed arrangements for maintenance and inspection

3.7.1 Traffic management

Close inspection or maintenance of the deck soffit over the waterway will require an underbridge unit and hence a single lane closure of the link road will be necessary.

3.7.2 Access

Over the waterway, the deck soffit can be accessed by underbridge unit from the carriageway above.

A minimum 2m wide maintenance platform is provided in front of the abutments. 1.5m minimum clear headroom is provided from the maintenance platform level to the precast beam soffit.

Inspection and maintenance of the remaining deck soffit, abutments and wing walls can be carried out from ground level using a platform or ladder to reach upper levels.

Foundations will not be visible or accessible for inspection.

3.8.1 Materials and finishes

Concrete	Element		Limiting Exposure Class
C48/60	Prestressed T beams		XD1
C40/50	Infill deck slab	Top Cantilever soffit Parapet plinths	XC3 XD3 XD3
C32/40	Abutment, exposed face below deck Abutment, wingwalls exposed side faces Abutment, wingwalls buried		XD1 XD3 DC-1
C32/40	CFA Piles		DC-4z. Note A
Note A			refore Design Chemical Class for nnical Summary Sheet for detail.
Reinforcemen	t All reinforcement to be bars to BS 4449:2005		grade 500B or 500C deformed
Parapets	Pair	nted (HA Type IV),	galvanised steel.

Backfill to abutments and retaining wallsFill material to structures to be Class 6N or 6P in accordance with DoT Specification for Highway Works.

Concrete Finishes

Deck soffit ie PC beam soffits F5 Surfaces to receive U4

waterproofing

Top of parapet plinth U3
Sides of parapet plinth F3
Abutment F2

Wingwalls F6 (grooved patterned profile finish)

Buried formed surfaces F1
Buried unformed surfaces U1

Protection

The top deck surface will be protected with a proprietary spray applied bridge deck waterproofing system to SHW Cl 2003.

All accessible concrete surfaces greater than 150mm below finished ground level to receive waterproofing to below ground concrete surfaces in accordance with the SHW CI 2004.

3.8.2 Sustainability issues

Conventional construction materials are proposed; therefore, no significant sustainability issues are foreseen.

3.9 Risks and hazards considered

Standard construction methods are anticipated with normally associated risks and hazards. A design hazard log and risk assessment process is active for the scheme.

3.10 Estimated cost of proposed structure together with other structural forms considered and the reasons for their rejection including comparative whole-life costs with dates of estimates.

The relative advantages, disadvantages and costs of various structural forms are discussed and appraised in Owen Williams reports No. 262701/012 'BHLR Structures Options Report'.

3.11 Proposed arrangements for construction

3.11.1 Traffic management

N/A

3.11.2 Service diversions

N/A

3.11.3 Interface with existing structures

N/A

4. DESIGN CRITERIA

4.1 Live loading, Headroom

4.1.1 Loading relating to normal traffic under AW regulations and C&U regulations

Full HA loading in accordance with BD 37/01

4.1.2 Loading relating to General Order traffic under STGO regulations

37.5 units of HB loading on any one notional lane only in accordance with BD 37/01.

4.1.3 Footway or footbridge live loading

Verge loading in accordance with BD 37/01

4.1.4 Loading relating to Special Order Traffic, provision for exceptional abnormal loads or indivisible loads, including location of vehicle track on deck cross-section

N/A

4.1.5 Any special loading not covered above

Approach embankments founded on soft ground will be subjected to advance works surcharging and/or ground treatment eg band drains or controlled modulus column installation, in advance of structural piling. Any residual lateral load or negative skin friction effects resulting from approach embankment loadings will be assessed and included in the design loadings for the bridge piled foundations.

4.1.6 Heavy or high load route requirements and arrangements being made to preserve the route, including any provision for future heavier loads or future widening.

N/A

4.1.7 Minimum headroom provided

The minimum headroom below bridge beams and concrete infill shall not be less than 1.5m after allowing for deflections arising from dead load, live load and settlement.

In addition, the soffit level of the deck shall be at a level greater than or equal to the 100 year flood level +20% flood flow plus 600mm freeboard.

4.1.8 Authorities consulted and any special conditions required

Authority Consulted	Special Requirement
1: British Telecom	1x90mm PVC duct required over structure.
2: EDF Energy 3: ESCC Planning	1x150mm duct required over structure.
4. ESCC	Planning Condition number 5. Bridge abutments are to be set back 2m from top of waterway channel banks to facilitate green corridor and soft bank solution.
5. Environment Agency	1.5m minimum maintenance headroom to underside of structure.
	600mm freeboard to be provided above water level during 100yr return period flood + 20% flood flow.

4.2 List of relevant documents from the TAS

See Appendix A

4.2.1 Additional relevant standards

BS 8500; Part 1; 2006 Concrete; Complementary British Standard to BS EN

206-1; Method of specifying and guidance for the

specifier

BS 8500; Part 2; 2006 Concrete; Complementary British Standard to BS EN

206-1; Specification for constituent materials and

concrete

CHE Memorandum

227/08

The Impregnation of Reinforced and Prestressed Concrete Highway Structures Using Hydrophobic Pore

Lining Impregnants

4.3 Proposed Departures from Standards given in 4.2 and 4.2.1

None

4.4 Proposed methods for dealing with aspects not covered by Standards in 4.2 and 4.2.1

N/A

5. STRUCTURAL ANALYSIS

5.1 Methods of analysis proposed for superstructure, substructure and foundations

The structure will be analysed in accordance with the recommendations given in PCA publication 'Integral abutments for prestressed beam bridges' by B.A Nicholson.

For the construction phase, the distribution of bending moments and shear forces in the deck will be determined by use of a simply supported line beam analysis.

For in service effects the deck analysis will be split into two stages. Firstly a grillage analysis will be undertaken assuming pinned supports at the abutments. The analysis will determine the maximum sagging moments in the deck, shear force distribution and vertical reactions. Transverse thermal and shrinkage effects will be considered in the design and appropriate measures taken to allow for these effects.

Secondly, a portal frame analysis of the deck and abutment stem walls will be undertaken, making allowance for the deck being monolithic with its supports and modelling soil structure interaction. The analysis will make allowance for the restraint to shrinkage and creep due to continuity over the supports. The analysis will return the maximum hogging moments in the deck and evaluate the rotation to be applied to the pileheads in the piled foundation design.

Load effects envelopes will be determined for the prestressed concrete beams which will be designed to Class 1 and Class 2 conditions.

Abutment stem walls will be designed for load effects determined from the portal frame analysis.

Retaining walls will be analysed by hand calculation.

Piled foundations will be analysed using appropriate industry standard software, considering a single representative pile and taking account of soil structure interaction effects including the lateral movements and rotational effects induced by deck load effects. Pile spacing is such that pile group effects are not considered to be appropriate.

Additional lateral loading on piles arising from potential approach embankment settlement will be analysed and added to pile loads arising from the deck and abutment analyses.

5.2 Description and diagram of idealised structure to be used for analysis.

Refer to Appendix D for diagram of idealised structure(s).

5.3 Assumptions intended for calculation of structural element stiffness

Element stiffness for concrete members will be determined in accordance with BS5400; Part 4; 1990; Clause 4.4 using full elastic uncracked member cross sections ignoring the presence of reinforcement.

Proposed earth pressure coefficients (k_a , k_0 , or k_p) to be used in the design of earth retaining elements

Earth pressure coefficients used in the calculation of lateral earth pressures at the rear of a full-height frame integral abutment will be calculated in accordance with the requirements and recommendations contained in BA 42/96 'The Design of Integral Bridges'. The earth pressure coefficients used in the calculation of the 'K^{*}' and 'at rest' earth pressures at the rear of the abutment shall be based on upper bound 6N granular backfill properties of density = $22kN/m^3$, maximum ø' = 45° , K_o = 0.6 and Kp = 12.6 when considering adverse effects

The earth pressure coefficients used in the calculation of the earth pressures at the rear of the cantilever wingwalls will be based on the guidance presented in "Integral Abutments for Prestressed Beam Bridges" by BA Nicholson 1998.

For the analysis of the free standing earth retaining wingwalls a representative peak angle of friction of 35° will be used, for which k_a = 0.27; k_p = 3.69 and k_0 = 0.43 (calculated in accordance with BD 30/87). k_a will be used for stability calculations and k_0 for structural element design.

6. GEOTECHNICAL CONDITIONS

6.1 Acceptance of recommendations of Section 8 of the Geotechnical Report to be used in the design and reasons for any proposed changes.

Section 2 of the Geotechnical Report has not been completed at this stage.

6.2 Geotechnical Report Highway Structure Summary Information (Form C)

A draft Geotechnical Report Highway Structure Summary sheet based on the information available in Part 1 of the Geotechnical Report is attached in Appendix C. A full Geotechnical Report Highway Structure Summary sheet and extracts from the completed Geotechnical Report Section 2 will be produced following development of the Geotechnical Report.

6.3 Differential settlement to be allowed for in the design of the structure.

The structure is founded on piles extending to the Ashdown Formation. A maximum differential settlement of 10mm between abutments will be considered.

6.4 If the Geotechnical Report is not yet available, state when the results are expected and list the sources of information used to justify the preliminary choice of foundations.

The preliminary choice of foundation is discussed in the draft Geotechnical Report Highway Structure Summary sheet contained in Appendix C. Part 2 of the Geotechnical Report, including Section 2 Highway Structures, is expected to be completed in Phase 2 of the project.

7. CHECKING

7.1 Proposed category of structure

Category 2 in accordance with BD2/05

7.2 If Category 3, name of proposed Independent checkers.

N/A

7.3 Erection proposals or temporary works for which an independent check will be required, listing parts of the structure affected with reasons for recommending an independent check.

N/A

8. DRAWINGS AND DOCUMENTS

8.1 List of drawings and documents accompanying the submission.

Appendix A List of relevant documents from TAS dated February 2009

Appendix B Drawing No Title

B1297000-PH1/1600.06a/9071 S07 Combe Haven Underbridge

AIP General Arrangement

Appendix C Geotechnical Information Draft Geotechnical Report Highway

Structure Summary Sheet.

Appendix D Idealised Structure



9	THE ABOVE IS SUBMITTED FOR ACCEPTANCE
9.1	Submission by designer
	Signed
	Name: P Blackie Position: Structures team leader, Jacobs Engineering Qualifications: BEng (Hons), CEng MICE
	Date 1710812
9.2	Endorsement by contractor
	Signed
	Name:
	Engineering Qualifications:
	Position:, Hochtief Vinci Joint Venture
	Date:
10.	THE ABOVE IS REJECTED/AGREED SUBJECT TO THE AMENDMENTS AND CONDITIONS SHOWN BELOW.
10.	
10.	
10.	CONDITIONS SHOWN BELOW.
10.	Reviewed
10.	Reviewed
10.	CONDITIONS SHOWN BELOW. Reviewed
10.	CONDITIONS SHOWN BELOW. Reviewed
10.	CONDITIONS SHOWN BELOW. Reviewed
10.	Reviewed
10.	CONDITIONS SHOWN BELOW. Reviewed



Appendix A List of Relevant Documents

Schedule of Design Documents Relating to Highway Bridges and Structures; February 2009

British Standards

BS 5268; Part 2; 2002	Structural Use of Timber			
BS 5400	Steel concrete and composite bridges			
Part 1; 1988	General Statement (see BD 1)			
Part 2; 1978	Specification for loads (see BD 1)			
Part 3; 2000	CP for design of steel bridges (see BD 1)			
Part 4; 1990	CP for design of concrete bridges (see BD 2)			
Part 5; 1979	CP for design of composite bridges (see BD 16)			
Part 9; 1983	Bridge bearings (see BD 20)			
Part 10; 1980	CP for fatigue (see BD 9)			
BS 5628; Part 1; 1992	Unreinforced Masonry			
BS 5930; 1999	Site Investigations			
BS 6031; 1981	Earthworks			
BS 8002; 1994	Earth retaining structures			
BS 8004; 1986	Foundations			
BS 8118; 1991	The structural use of aluminium			
BS EN 1317-1-1998; Road Restraint Systems – Part 1	Terminology and general criteria for test methods			
BS EN 1317-2-1998; Road Restraint Systems – Part 2	Performance classes, impact test acceptance criteria and test methods for safety barriers			
BS EN 1317-3-2000; Road Restraint Systems — Part 3	Performance classes, impact test acceptance criteria and test methods for crash cushions			
DD ENV 1317-4-2002; Road Restraint Systems – Part 4	Terminals and transitions			
BS-EN-14388; 2005	Road traffic noise reducing devices - Specification			

Miscellaneous

Circular Roads No 61/72 - Routes for heavy and high abnormal loads.

Railway Group Approved Code of Practice GC/RC5510: Recommendations for the Design of Bridges (2000) (for full list of other Network Rail Standards, refer to RSSB, Railway Safety and Standards Board)

Simplified Tables of External Loads on Buried Pipelines (1986)

Traffic Management Act 2004

The Manual of Contract Documents for Highway Works (MCDHW)

Volume 1:Specification for Highway Works 1998, including amendments to November 2007

Volume 2:

Notes for Guidance on the Specification for Highway Works 1998, including amendments to

November 2007

Volume 3:

Highway Construction Details 1991, including amendments to May 2007

The Design Manual for Roads and Bridges (DMRB)

Bridges and Structures (BA Series)

Reproduced on following pages

Bridges and Structures (BD Series)

Reproduced on following pages

Bridges and Structures, Technical Memoranda (BE Series)

Reproduced on following pages

Traffic Engineering and Control, Standards (TD Series)

TD 9/93

Road layout and geometry. Highway link design

TD 19/06

Requirement of Road Restraint Systems & correction No. 1

TD 27/05

Cross Sections and headroom

TD 36/93

Subways for pedestrians and cyclists, layout and dimensions

Highways, Advice Notes (HA Series)

HA 59/92

Mitigating Against Effects on Badgers

HA-80/99

Nature Conservation Advice in Relation to Bats

HA 84/01 (1)

Nature Conservation and Biodiversity

HA 97/01

Nature Conservation Management Advice in Relation to Dormice

HA-98/01

Nature Conservation Management Advice in Relation to Amphibians

Highways, Standards (HD Series)

HD 22/08

Managing Geotechnical Risk

	ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES)
BA-9/81	The Use of BS 5400: Part 10: 1980. Code of Practice for Fatigue Amendment No. 1
BA-16/97	The Assessment of Highway Bridges and Structures. Amendment No. 1 Amendment No.2
BA-19/85	The Use of BS 5400: Part 3: 1982
BA 24/87	Early Thermal Cracking of Concrete Amendment No. 1
BA 26/94	Expansion Joints for Use in Highway Bridge Decks
BA 28/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BA 30/94	Strengthening of Concrete Highway Structures Using Externally Bonded Plates
BA-34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BA 35/90	Inspection and Repair of Concrete Highway Structures
BA 36/90	The Use of Permanent Formwork
BA 37/92	Priority Ranking of Existing Parapets
BA-38/93	Assessment of the Fatigue Life of Corroded or Damaged Reinforcing Bars
BA 39/93	Assessment of Reinforced Concrete Half-joints
BA 40/93	Tack Welding of Reinforcing Bars
BA 41/98	The Design and Appearance of Bridges
BA 42/96	The Design of Integral Bridges [Incorporating Amendment No. 1 dated May 2003]
BA 43/94	Strengthening, Repair and Monitoring of Post-tensioned Concrete Bridge Decks
BA 44/96	Assessment of Concrete Highway Bridge and Structures
BA 47/99	Waterproofing and Surfacing Concrete Bridge Decks
BA 50/93	Post-tensioned Concrete Bridges: Planning, Organisation and Methods for Carrying Out Special Inspections
BA 51/95	The Assessment of Concrete Structures Affected by Steel Corrosion
BA 52/94	The Assessment of Concrete Highway Structures Affected by Alkali Silica Reaction
BA 53/94	Bracing Systems and the Use of U-Frames in Steel Highway Bridges
BA 54/94	Load Testing for Bridge Assessment
BA 55/06	The Assessment of Bridge Substructures and Foundations, Retaining Walls and Buried Structures
BA 56/96	The Assessment of Steel Highway Bridges and Structures
BA 57/01	Design for Durability
BA-58/94	Design of Bridges and Concrete Structures with External Unbonded Prestressing
BA 59/94	Design of Highway Bridges for Hydraulic Action
BA-61/96	The Assessment of Composite Highway Bridges
BA-67/96	Enclosure of Bridges
BA 68/97	Crib Retaining Walls
BA 72/03	Maintenance of Road Tunnels

	ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES)
BA-74/06	Assessment of Scour at Highway Bridges
BA 80/99	Use of Rock Bolts
BA-82/00	Formation of Continuity Joints in Bridge Decks
BA-83/02	Cathodic Protection for Use in Reinforced Concrete Highway Structures
BA 84/02	Use of Stainless Steel Reinforcement in Highway Structures
BA 85/04	Coatings for Concrete Highway Structures & Ancillary Structures
BA-86//06	Advice Notes on the Non-Destructive Testing of Highway Structures
BA-87//04	Management of Corrugated Steel Buried Structures
BA-88//04	Management of Buried Concrete Box-Structures
BA 92/07	The Use of Recycled Concrete Aggregates in Structural Concrete
BA-93/09	Structural Assessment of Bridges with Deck Hinges
	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD 2/05	Technical Approval of Highway Structures
BD-7/01	Weathering Steel for Highway Structures
BD 9/81	Implementation of BS 5400: Part 10: 1980. Code of Practice for Fatigue
BD-10/97	Design of Highway Structures in Areas of Mining Subsidence
BD-12/01	Design of Corrugated Steel Buried Structures with Spans Greater than 0.9 Metres and up to 8.0 Metres
BD 13/06	Design of Steel Bridges. Use of BS 5400: Part 3: 2000
BD 15/92	General Principles for the Design and Construction of Bridges. Use of BS 5400: Part 1: 1988
BD-16/82	Design of Composite Bridges. Use of BS 5400: Part 5: 1979 Amendment No. 1
BD 20/92	Bridge Bearings. Use of BS 5400: Part 9: 1983
BD-21/01	The Assessment of Highway Bridges and Structures
BD 24/92	Design of Concrete Bridges. Use of BS 5400: Part 4: 1990
BD-27/86	Materials for the Repair of Concrete Highway Structures
BD 28/87	Early Thermal Cracking of Concrete Amendment No. 1
BD 29/04	Design Criteria for Footbridges
BD 30/87	Backfilled Retaining Walls and Bridge Abutments
BD-31/01	The Design of Buried Concrete Box and Portal Frame Structures
BD 33/94	Expansion Joints for Use in Highway Bridge Decks
BD-34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BD-35/06	Quality Assurance Scheme for Paints and Similar Protective Coatings
BD 36/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BD 37/01	Loads for Highway Bridges

	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD 41/97	Reinforced Clay Brickwork Retaining Walls of Pocket Type and Grouted Cavity type Construction Use of BS 5628: Part 2: 1995
BD-42/00	Design of Embedded Retaining Walls and Bridge Abutments
BD-43/03	The Impregnation of Reinforced and Prestressed Concrete Highway-Structures using Hydrophobic Pore-Lining Impregnants
BD-44/95	The Assessment of Concrete Highway Bridges and Structures
BD 45/93	Identification Marking of Highway Structures
BD-46/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures [Stage 2 - Modern Short Span Bridges]
BD 47/99	Waterproofing and Surfacing of Concrete Bridge Decks
BD-48/93	The Assessment and Strengthening of Highway Bridge Supports
BD-49/01	Design Rules for Aerodynamic Effects on Bridges
BD-50/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures Stage 3 — Long Span Bridges
BD 51/98	Portal and Cantilever Signs/Signal Gantries
BD 53/95	Inspection and Records for Road Tunnels
BD 54/93	Post-tensioned Concrete Bridges, Prioritisation of Special Inspections
BD 56/96	The Assessment of Steel Highway Bridges and Structures
BD 57/01	Design for Durability
BD-58/94	The Design of Concrete Highway Bridges and Structures with External and Unbonded Prestressing Design of Highway Bridges for Vehicle Collision Loads
BD 60/04	Design of Highway Bridges for Vehicle Collision Loads
BD 61/96	The Assessment of Composite Highway Bridges
BD 62/07	As Built, Operational and Maintenance Records for Highway Structures
BD 63/07	Inspection of Highway Structures
BD 65/97	Design Criteria for Collision Protector Beams
BD-67/96	Enclosure of Bridges
BD-68/97	Crib Retaining Walls
BD-70/03	Strengthened/Reinforced Soils and Other Fills for Retaining Walls and Bridge Abutments Use of BS8006: 1995, incorporating Amendment No. 1 (Issue 2 March 1999)
BD 74/00	Foundations
BD 78/99	Design of Road Tunnels
BD 79/06	The Management of sub-Standard Highway Structures
BD-81/02	Use of Compressive Membrane Action in Bridge Decks
BD-82/00	Design of Buried Rigid Pipes
BD-84/02	Strengthening of Concrete Bridge Supports Vehicle Impact Using Fibre Reinforced Polymers
BD-85/08	Strengthening Highway Structures Using Externally Bonded Fibre Reinforced Polymer
BD-86/07	The Assessment of Highway Bridges and Structures For The Effects of Special Types General Order (STGO) and Special Order (SO) Vehicles
BD 87/05	Maintenance Painting of Steelwork

	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD-89/03	The Conservation of Highway Structures
BD-90/05	Design of FRP Bridges and Highway Structures
BD-91/04	Unreinforced Masonry Arch Bridges
BD-94/07	Design of Minor Structures
BD 95/07	Treatment of Existing Structures on Highway widening Schemes
	TECHNICAL MEMORANDA - BRIDGES (BE SERIES)
BE 13	Fatigue Risk in Bailey Bridges
BE-23	Shear Key Decks Amendment No. 1 to Annex
BE-5/75	Rules for the Design and Use of Freyssinet-Concrete Hinges in Highway Structures
BE 7/04	Departmental-Standard (Interim)
	Motorway-Sign/Signal Gantries
	INTERIM ADVICE NOTES (IAN)
IAN 117/08 Rev 1	Gertification of combined kerb and drainage products
IAN 116/08	Nature conservation advice in relation to bats
IAN-104/07	The Anchorage of Reinforcement and Fixings in Hardened Concrete
IAN 97/07	Assessment and upgrading of existing parapets
IAN 96/07r1	Guidance on implementing Results of Research on Bridge Deck Waterproofing
IAN 95/07	Revised Guidance Regarding the Use of BS8500(2006) For the Design and Construction of Structures Using Concrete
IAN 91/07	Interim Advice on the identification of "Particularly at Risk" supports
IAN 70/06	Implementation of New Reinforcement Standards
IAN 69/05	Design for Maintenance
IAN 48/03	Measures To Minimise The Risk of Sulphate Attack (Including Thaumasite) - New Construction and Structures Under Construction
IAN-47/02	Post Tensioned Grouted Duct concrete Bridges
IAN 41/02	European Cement Standards
IAN 05/96	BD 24/92 The Design of Concrete Highway Bridges and Structures. Use of BS 5400: Part 4:1990

BD 44/95 The Assessment of Concrete Highway Bridges and Structures

BA 50/93 Post Tensioned concrete Bridges

IAN-04/96

IAN-03/96

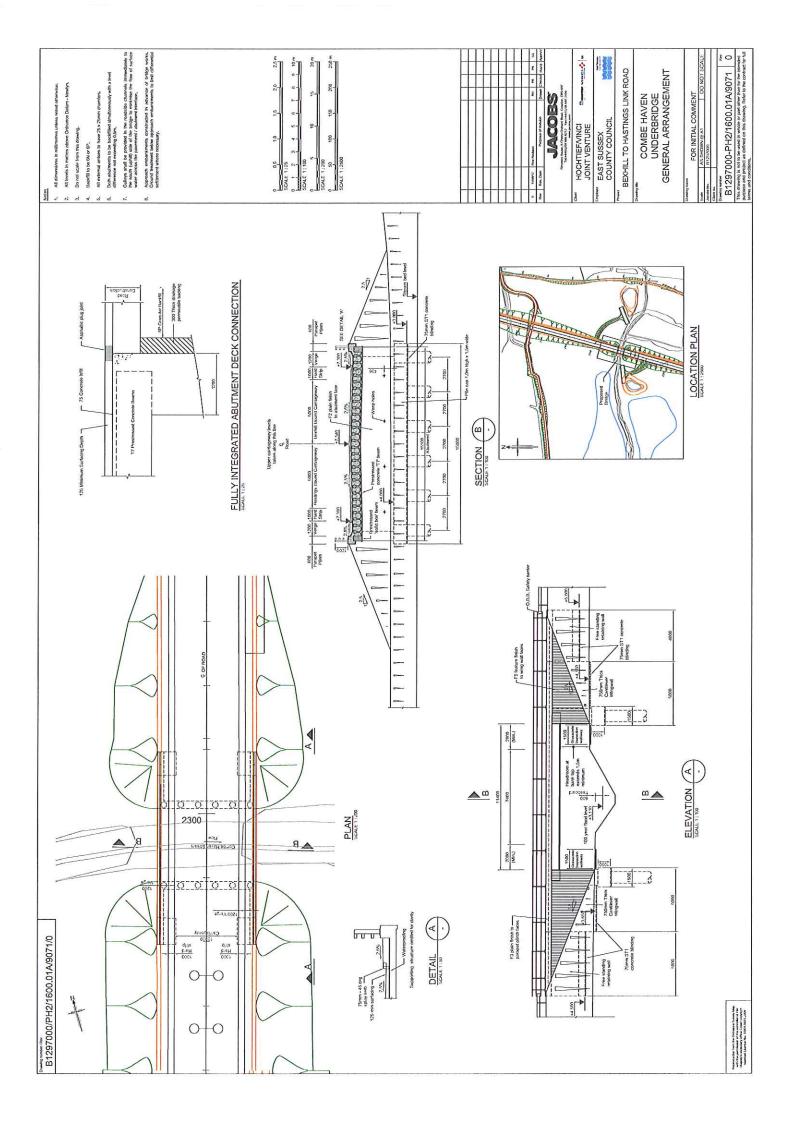
Appendix B Drawings

Drawing No

Title

B1297000-PH1/1600.06a/9071

S07 Combe Haven Underbridge AIP General Arrangement



Appendix C Geotechnical Information

August 2012

BEXHILL TO HASTINGS LINK ROAD

GEOTECHICAL SUMMARY INFORMATION

STRUCTURE NAME	CHAINAGE and OS Grid Reference				
S07 - Combe Haven Underbridge	Ch 2300 OS: 574843.8E, 110012.5N				
Rev: 2	DESIGN LIFE: 120 years				
SOILS/GEOLOGY	RELEVANT EXPLORATORY HOLES: BH116, BH117 (URS Investigation, 2009)				
Strata	Typical depths				
Alluvium Ashdown Formation	4.47 to -0.97 m OD below -0.97m OD				
PREVIOUS GROUND HISTORY		Agricultural Land			
CONTAMINATED GROUND RISK ASSESSMENT REQUIRED No			No		

GROUNDWATER

Groundwater was encountered initially at levels between 2.73m OD (1.1m bgl – BH116) and 3.27m OD (1.2m bgl – BH117) within Alluvium and rose only in BH116 to level of 2.93m OD (0.9m bgl) after 20 minutes. A second groundwater strike encountered confined groundwater within Ashdown Formation at levels between -0.97m OD (4.8m bgl – BH116) and -2.53m OD (6.7m bgl – BHH117) and rose to levels of between -2.23m OD (6.7m bgl – BH117) and 3.43m OD (0.4m bgl – BH116) in 20 minutes. A third confined groundwater was encountered within the Ashdown Formation in BH117 at a level of -3.93m OD (8.4m bgl) and rose to a level of 2.47m OD (2m bgl) after 20 minutes. No monitoring was carried out.

Allowing for seasonal fluctuations, the preliminary design groundwater level is assumed to be at foundation level.

EARTH PRESSURE VALUE K₀* K_a* Kp*

See Section 5.4 of the AIP.

TYPE OF FOUNDATION	Pile Foundation				
BEARING CAPACITY	N/A	N/A			
Structure Element	Founding Stratum	Founding Level (m OD)	Footing Size	Allowable Bearing Pressure (kN/m2)	

PILE DESIGN							
Structure Element	Founding Stratum	Toe Level (m OD)	Pile dia (m)	Pile length (m)	Pile working Load (kN)		
East and West abutment	Ashdown Formation	East abutment = -14 West abutment = -14.5	0.9	17.0	1600		

Note: Pile lengths and toe levels are approximate.

Pile type: CFA

Criteria for selecting pile toe level: Pile capacity

Allowance for negative skin friction within design: Yes

SETTLEMENT

Differential settlement to be allowed for between adjacent supports: 10mm

Differential settlement to be allowed between structure and approach embankment: 20mm (within 10 metres of the interface between structures and approach embankments)

CHEMICAL ANALYSIS

Buried Concrete classification:

The results of chemical tests on soil samples taken within the rural areas indicate pH values ranging between 3.8 to 9.4 and sulfates (2:1 Water Extract) values of between 10 to 900mg/l. The recommended Design Sulfate and Concrete Classification based on BRE Special Digest 1 (2005) are DS-2 and AC-3z respectively.

NOTES

- 1. The ground sequence at the site is Top Soil, Alluvium and Ashdown Formation. The boreholes indicate the maximum combined thickness of Top Soil and Alluvium to be 5.50m.
- 2. Based on the formation level, the structure will likely be founded on soft Alluvium layer, which is underlain by stiff clays, dense sands of the Ashdown Formation. The low shear strength of the Alluvium layer prevents its use as a bearing stratum. The risk of excessive settlements and failure is high. To transfer the structural loads to the competent stiff to very stiff /very weak to weak interbedded Ashdown Formation, pile foundations are recommended.
- 3. The behaviour of the groundwater indicates likely presence of confined aquifer. This should be considered during construction.

Contract No: 49325727

Bexhill - Hastings Link Road Project:

Client:

East Sussex County Council

BH116

Glient	E	ast Sussex C	oun	ty Cou	ıncil								
SAM		In situ TESTS	. to										
Depth	Type/ No.	SPT/U4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thick- ness)			DESCR	RIPTION			Instru- ment/ Backfill
0.15 0.30	D1 D2		\$\brace{\	3.33		-0.50	Soft, dark brown o Occasional rootlet (TOPSOIL)	orange brov is.	vn mottled	slightly sar	ndy silty CL	AY. Sand is fine.	
0.50 IICALVFACTUAL REPOR	D3		1 1 1 1		×		Soft, grey to red b silty CLAY, Sand i (ALLUVIUM)	rown, occa s fine.	sional orar	nge and gre	ey mottled s	slightly sandy	
Client C	B5 U1X	(5 - 0mm)	*		x	-							
2.00 2.00	U1 D6	(30 - Unrecorded)		1.83		2.00	Soft light grey gree (ALLUVIUM)	en fine san	dy CLAY.			17.49	
2.50	D7 SPT8 B9	N=16 (3/3/4/3/4/5)		1.33		2.50	Stiff to very stiff, fi are stained grey, o (ASHDOWN BED	orange brow	nly laminat vn and bla	ed yellow b ck.	orown CLAY	/. Laminations	
3.00	U3	(44 - Unrecorded)		-		-							
3.50	D10 B11					-							
4.00 EHOPE FOO	U4	(50 - Unrecorded)		-		-							
BOO 4.50	D12 SPT13 B14	N=30 (3/3/6/6/12/6)	<u>\$</u>	-0.97		4.80	Slightly sandy and Dense, yellow brostained black and	-					
5.00	D15			-		-	stained black and weak sandstone, (ASHDOWN BED		wn, angula	ar to suban	gular, fine t	to coarse very	
5.50	B16			-		-							
6.00	D17 SPT18	N=31 (6/16/13/6/5/7)		-		-							
6.50 Date	B19					-	Sand is silty from (
74 34 34 34 34 34 34 34 34 34 34 34 34 34		g Progress and Mole Cas'g Cas'g			10000	1000	Chiselli	, · · · · · · ·		Added		GENERAL	
Date 16/01/09 16/01/09 17/01/09 17/01/09 Logged by IR	11me 14.00 16.30 0 08.00	Hole Cas'g Cas'g Depth Dia 1.10 0.00 150 4.50 3.00 150 4.80 3.00 150	1.1 0.4 0.4 4.8	oth to 0 0.90 0 0	(mins		From To	Time (hh:mm)	From	То	Draft 150mm c U100 san	REMARKS assing to 3.0m bgl. apples taken using gging no visible or evidence of contar veathering interpre aks et al. 1993: (V)).	
Checked I	oy:	Equipment: Cable Percussion R	ig - Da	ando 200	0								
Status: Southern Testing Laboratories Ltd						109986.7 N mAOD 17/12/2008 End Sheet 1 of 3							

Contra	ct No: 4	932	5727											TUR	S	
Project	: Е	3exhi	II - Ha	sting	gs L	ink R	oad						l	Record of Bore	hole	
Client:	E	East S	Susse	х Со	unt	у Соц	ncil							BH11	6	
SAME			situ TE		. 50					STRA	TA					
Depth	Type/ No.		SPT/U4 (Blows)			Reduced Level (mOD)	Legend	Depth (Thick- ness)			DESCR	RIPTION			Instru- ment/ Backfill	
8.20	SPT20 B21		N=6 (3/4/0/0/3/3	9)		-		-	Loose at 8.2m bg	1.						
9.00	SPT22 B23		N=30 (4/9/14/5/4/	7)					Dense at 9.0m bg	al.						
10.00	SPT24		N=42 (4/6/6/7/10/1	9)				-	Dense at 10.0m b	ogl.						
10.50	B25		N=84	0/201		-7.17	×	11.00	Very dense yellov	y brown san	dy SILT a	nd lithorelic	s of subang	gular fine to		
11.50	SPT27	(10	0/16/18/16/2	2/28)		-7.67	× · · · · · · · · · · · · · · · · · · ·	_11.50	Very dense yellow brown sandy SILT and lithorelics of subangular fine to medium very weak sandstone. Sand is fine. (ASHDOWN BEDS) Very stiff, light to dark grey CLAY and frequent lithorelics of angular to subangular fine to coarse mudstone.							
12.50	D29 SPT30 B31	(N=38 (12/12/8/7/9/14)						subangular fine to	o coarse mu OS)	dstone.					
13.50	D32							-								
14.00	SPT33	(7	N=80 7/9/10/20/26	/24)		-10.17		14.00	Very weak, thinly MUDSTONE. Pa (ASHDOWN BED	laminated d tially weath OS)	lark grey a ered to a	ey angular to subangular, fine to coarse o a very stiff grey clay.				
14.50	B34					-		-								
	Borir	ıg Pro	gress						Chisell		Water	· Added		GENERAL		
Date	Time	Hole Depth	Cas'g	Cas'g		er Ros	e Time	Sealed	From To	Time (hh:mm)	From	То	Draft 150mm o U100 sar weight During lo olfactory Zone of v from Spir (III); (II);(I	REMARKS casing to 3.0m bgl. inples taken using or gging no visible or evidence of contan weathering interpret iks et al. 1993: (V);).	double nination. ed from (IV);	
Logged by: JB Cohecked by: CAB Status: Dreft Contractor: Southern Testing Laboratories Ltd									55.5 E 86.7 N	Ground L 3.83 mAOD	.evel:	Date: 16/12/200 17/12/200		Scale: 1:40.0 Sheet 2 of 3		

9 12:28:00	Contra	ct No: ∠	19325	5727											TUR	S
1: 14/08/200	Project	: [Bexhil	I - Hast	ing	s L	ink Ro	oad							Record of Borel	
PJ Printe	Client:			Sussex											BH11	6
URS ALL	SAME			itu TEST							STRA	ATA				
ILL - HASTINGS	Depth	Type, No.		SPT/U4 (Blows)		Water	Reduced Level (mOD)	Legend	Depth (Thick- ness)				RIPTION			ment/
TECHNICAL/FACTUAL REPORT DATA/GINT/BEX	15.50	D35 SPT36 B37	(8/14/	N=>65 15/19/31/75mn	√-)		-		-							
25727 BEXHILL TO HASTINGS LINK ROADIT	17.00	D38 SPT39	(15/2	N=>28 12/28/75mm/- <i>I-I</i>	<u>'-)</u>	1	-12.97 - - -13.57			Very weak, thin weathered MUI (ASHDOWN BI	EDS)	y Newton &	x 50 00000 50		fine to coarse	
SI/W: DEPHILL DORCHOELEO FIN: JUEDREPORD, DESELVAT SUBSECT SUB										Oli			r Added		OENEDA	
01234 3490	Date	Time	Hole	Cas'g Ca Depth D	s'g	Wate Dept	er Rose		Sealed	Chise From To	Time	From			GENERAL REMARKS	
Lid Home Line Bedford MK40 1TS Telephone: 01234 349641 www.URSCorp.com	17/01/09		17.40	3.00 15	_	0.40		(mins	(in)	16.80 17.0 17.00 17.4	0 00:15		. 02 50	Draft 150mm of U100 sar weight During lo olfactory Zone of v from Spir (III); (II);(I	casing to 3.0m bgl. imples taken using d gging no visible or evidence of contam veathering interprete taks et al. 1993; (V);).	louble sination. ed from (IV);
	Logged by: JB		Equipn Cable I	nent: Percussion	Rin	- Da	ndo 2000	0	Location		Ground L 3.83	.evel:	Date: 16/12/200	8 Start	Scale: 1:40.0	
Corpor	Checked by CAB Status:	y:	Contra	ctor:					Action to the second	55.5 E 86.7 N	mAOD		17/12/200		W 10. (10.2.30. 10.	
٤Į	Draft		Southern Testing Laboratories Ltd												Sheet 3 of 3	

NO 12.45.15	Contrac	ct No: 49	9325727							UR	S
D. 14/US/20	Project	В	exhill - Hasting	gs L	ink R	oad				Record of Bore	hole
CHO.	Client:	E	ast Sussex Co	ount	у Соц	ıncil				BH11	7
UKS ALL	SAME		In situ TESTS					STRA	TA		
HASTINGS	Depth	Type/ No.	SPT/U4 (Blows)	Water	Reduced	Legend	Depth (Thick-		DESCRIPTION		Instru- ment/ Rackfill
CIN INCOME.	0.10 0.20	CS1 CS2			(mOD)	111211	ness)	Soft, medium brown, slightly s (TOPSOIL)	sandy CLAY with frequ	uent rootlets.	
EPORT DATA	0.50	CS3			3.97	111511	0.50	Soft, thickly laminated, orange mottles and rootlets. Sands a	e/brown sandy CLAY v	with occasional grey/brown	
V-ACTUAL R					3		-	(ALLUVIUM)	e ilile.		
VIECHNICAL	1.00	CS4		₹	3.17		1.30	Becoming slightly sandy from		Account of ability	
S LINK KOAL	1.30	D5 U6	(9 - 400mm)		3		-	Soft, very closely fissured, mo sandy CLAY with rare rootlets (ALLUVIUM)	ottled grey/brown and o	orange/brown, slightly	
TO HASTING		67		3	2 47		2.00		fi CLAVith	dada assassinas	
5727 BEXHILL	2.00	D7		-		邑	-	Firm, very closely fissured, grataining. (ALLUVIUM)	rey/brown CLAY, With	rare, dark drange iron	
OUNCILW932	2.50	U8	(15 - 450mm)		8		(1.00)				
X COUNTY C	3.00	D9	N=6		1.47		3.00	Soft, very closely fissured, blu	re/grey CLAY, with rar	e orange/brown mottles.	
T SUSSE		SPT10	(1/0/1/1/2/2)				-	(ALLUVIUM)			
SP-JOBSIEVE	3.30 3.50	D11 U12	(50 - 450mm)		8		(1.00)				
Ile: J:\BEDFOF		D.10			0.47		4.00			Alaman Cl AV	
TOLE LOG FI	4.00	D13			ä	臣	-	Firm, very closely fissured, m (ALLUVIUM)	ottled blue/grey and o	range/brown CLAY.	
XHILL BORE	4.50	U14	(50 - 450mm)		3	喜	(1.00)				
Style: BEXHIL	5.00	D15	N=25		-0.53		5.00	Stiff, very closely fissured, blu	ue/brown/arev CLAY. v	with frequent blue/grey	
	3222	SPT16	(2/4/5/6/6/8)		N		-	mottling. (ASHDOWN BEDS)	37		
	5.45 5.50	D17 U18	(60 - 450mm)		1.03		_5.50	Stiff, fissured, thinly laminated rare patches of orange/brown (ASHDOWN BEDS)			
	6.00	D19			-1.53	昌	6.00	Becoming light blue/grey CLA Stiff, very closely fissured, blu medium, sub-angular, blue/gr			- ////
			1200 44 - 221 - 222 - 242			薑	-	(ASHDOWN BEDS)	ey mudstone.		
	6.50	U20	(80 - 450mm)	Ž 3		匿	-				
E	7.00	D21 SPT22	N=36 (5/9/12/8/8/8)	<u></u>		臣	-				
RSCorp.co.		W22				E					
3641 www.L	7.50	U23 Borine	g Progress and	Wat	er Obs	⊢ — - ervatio	ns	Chiselling	Water Added	GENERAL	V////

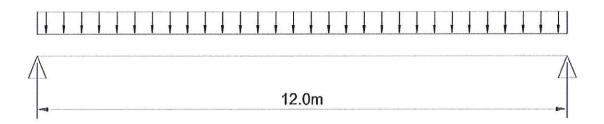
7.00	SPT22 W22		(5/9/12/8/8/					-							
Boring Progress and Water Observations										Chiselling Water Ad					GENERAL
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose	Time (mins)	Sealed (m)	From	То	Time (hh:mm)	From	То	Draft	REMARKS
06/01/09 06/01/09 06/01/09 07/01/09	16.00 16.20	1.20 7.00 7.00 7.00 7.00	0.00 4.00 4.00 4.00	150 150 150 150 150	1.20 7.00 6.70 1.40	6.70	20	()						150mm of During lo olfactory Chiseled - 9.6m. Zone of v	easing to 4.0m bgl. gging no visible or evidence of contamination. from 9.0 - 9.35m and 9.55 weathering interpreted from nks et al. 1993: (V); (IV);
Logged by: HH Checked by: CAB Status:									: 36.5 E 35.3 N		Ground Level: 4.47 mAOD		Date: 06/01/2009 Si 07/01/2009 Ei		Scale: 1:40.0 Sheet 1 of 2

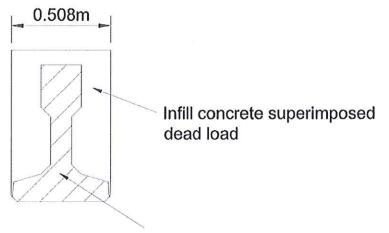
Contra	ict No: 4	9325727								***************************************		UR	S
Project	t: E	exhill - H	asting	gs L	ink R	oad						Record of Bore	ehole
	Е	ast Susse	ex Co	unt	у Соц	ıncil		·····				BH11	7
SAMI	PLES 8	k In situ T	ESTS	Ļ					STRATA				
Depth	Type/ No.	SPT/U (Blows		Water	Reduced Level (mOD)	Legend	Depth (Thick- ness)		DESC	RIPTION			Instru- ment/
8.00 8.30 8.40 8.50	D24 D25 W26 U27	(120 - 300)	mm)	3	-3 83 -4 33		8.30 - - 8.80	Lithorelics of mudst bgl. Stiff very closely fiss lithorelics of weak d MUDSTONE. (ASHDOWN BEDS	sured grey-blue m dark blue-grey sub	ottled orange-b angular to sub-	rown CL rounded	AY with frequent fine to medium	
9.00 9.35	D28 SPT29 B30 SPT31	N=100 (18/7/20mm/20/50/ N=60 (25/50mm//40/60	/30/30mm/	-)	-5 13	- 0 0 0	9.60	Very dense orange/ coarse, angular SAI (ASHDOWN BEDS	NOSTONE.	r nequent nunor	elics of v	veak, medium to	
SAMK Depth 8.00 8.30 8.40 8.50 9.00 9.35									End of Bore	ehole at 9.60m			
Date		g Progress						Chisellin		r Added		GENERAL	1
Date 07/01/09 07/01/09	09.00	Hole Cas'g Depth Depth 8.40 4.00 9.60 4.00	Cas'g Dia 150 150	8.40 2.00	th to 2.00	(mins		From To 9.30 9.35 9.55 9.60	Time (hh:mm) From 00:15 00:15		Oraft 50mm c Ouring loo Ifactory Chiseled	REMARKS asing to 4.0m bgl. gging no visible or evidence of contam from 9.0 - 9.35m ar veathering interpret ks et al. 1993: (V);	
Logged by:		Equipment: Cable Percus	sion Ric	- Do	ndo 200	0	Location		Ground Level:	Date: 06/01/2009	Start	Scale:	
Checked by CAB Status: Draft	,,	Contractor: Southern Test				_	1		1.47 nAOD	07/01/2009	5684 8	1:40.0 Sheet 2 of 2	

Appendix D Idealised Structure

Step 1 Simply supported line beam analysis

- Determine dead and superimposed dead bending moment and shear force distributions.
- 0.508m width beam

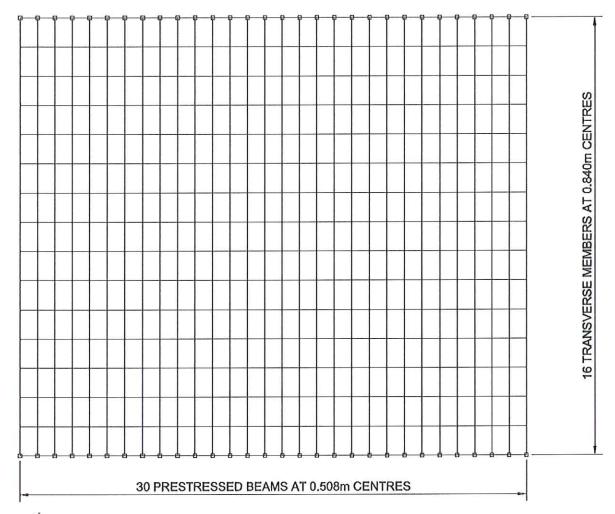




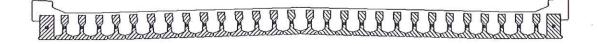
Prestressed beam dead load

Step 2: Grillage analysis of deck

- Determine live loading combinations 1 and 3 maximum sagging moment
- Determine live loading combinations 1 and 3 shear force distributions
- Determine vertical deck design load for piles

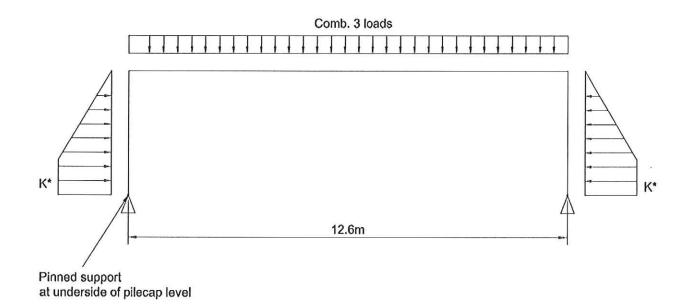


□ PINNED END SUPPORT



Step 3: Soil structure interaction analysis

- 0.508m width of deck
- Apply combination 3 live loads to deck and passive earth pressures to abutments
- Determine hogging moments at beam ends
- Determine bending moments for pile design
- Determine bending moment and shear force distribution in abutment stem walls



Step 4: Pile design

Abutment movement and rotation applied to pileheads

